Investigations on birefringence effects in polymer optical fiber Bragg gratings

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ABSTRACT

Step-index polymer optical fiber Bragg gratings (POFBGs) and microstructured polymer optical fiber Bragg gratings (mPOFBGs) present several attractive features, especially for sensing purposes. In comparison to FBGs written in silica fibers, they are more sensitive to temperature and pressure because of the larger thermo-optic coefficient and smaller Young’s modulus of polymer materials. (M)POFBGs are most often photowritten in poly(methylmethacrylate) (PMMA) materials using a continuous-wave 325 nm HeCd laser. For the first time to the best of our knowledge, we study photo-induced birefringence effects in (m)POFBGs. To achieve this, highly reflective gratings were inscribed with the phase mask technique. They were then monitored in transmission with polarized light. For this, (m)POF sections a few cm in length containing the gratings were glued to angled silica fibers. Polarization dependent loss (PDL) and differential group delay (DGD) were computed from the Jones matrix eigenanalysis using an optical vector analyser. Maximum values exceeding several dB and a few picoseconds were obtained for the PDL and DGD, respectively. The response to lateral force was finally investigated. As it induces birefringence in addition to the photo-induced one, an increase of the PDL and DGD values were noticed.

Keywords: Polymer optical fiber, Bragg grating, birefringence, transverse force, sensor

1. INTRODUCTION

Fiber Bragg gratings (FBGs) were first fabricated in polymer optical fibers (POFs) in 19991. Since then, Polymer optical FBGs have been photo-inscribed point-by-point2 and with the phase mask technique, including single exposure3-5 and laser beam scanning6,7. FBGs inscribed in POFs present several attractive features for sensing purposes. Compared to their counterparts produced in silica fibers, they are more sensitive to temperature and pressure because of the larger thermo-optic coefficient and smaller Young’s modulus of polymer materials8-13. Besides, PMMA demonstrates absorption of moisture up to 2 w.t. %, so that PMMA FBGs can be used as humidity sensors14, biochemical concentration sensors15 or water detection sensors16. Although different polymer materials can be used to manufacture POFs17-19, poly(methyl methacrylate) (PMMA) is the most often encountered one.

The step-index POFs used in this work were supplied by the Hong Kong Polytechnic University. The cladding is in pure PMMA while the core is composed of PMMA doped with diphenyl sulfide (5% mole) and trans-4-stilbenemethanol (1% w.t.). The mPOFs were supplied by the Technical University of Denmark, and were produced using undoped PMMA with a hexagonal structure of three rings in the inner cladding. 6 mm long step-index POFBGs and 5 mm long mPOFBGs with high reflectivity were photo-inscribed thanks to a helium-cadmium laser emitting at 325 nm with the scanning phase mask technique20,21.

In this paper, for the first time to the best of our knowledge, we studied photo-induced birefringence effects in (m)POFBGs arising from both the lateral inscription process and the application of a transverse force. After photo-inscription, (m)POF sections with gratings were UV-glued or connected to silica fibers on both sides of (m)POFs, and then birefringence effects were monitored in transmission with polarized light.

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Like in silica fiber, the lateral writing process in (m)POF induces a small quantity of birefringence that combines with the intrinsic fiber birefringence and leads to polarization effects within the grating. This small amount of birefringence causes the orthogonal polarization modes to experience different couplings through the grating. In the presence of birefringence, the resulting transmitted spectrum is then the combination of two overlapping, offset but otherwise identical spectra. Because these two spectra cannot be generally distinguished due to the limited resolution of the measurement devices, two measurements of polarization dependent loss (PDL) and differential group delay (DGD) were made. They were both computed from the Jones matrix eigenanalysis method using an optical vector analyzer (OVA CTe from Luna Technologies, attesting that the photo-induced birefringence resulting from the side inscription process is \(7 \times 10^{-6}\) for the step-index POFs.

Finally, the response to lateral force in the range (0 - 0.75 N) was investigated on gratings written in step-index POFs with an experimental set-up allowing the application of controlled transverse loads on the gratings. As it induces mechanical birefringence in addition to the photo-induced one, a drastic increase of the PDL was noticed.

2. EXPERIMENTAL SET-UP

The step-index POFBGs were manufactured at the University of Mons. The laser used in this work is a He-Cd laser (Kimmon IK57511-G) with an output power of 30 mW at 325 nm. The output beam width of the laser is 1.2 mm. Figure 1 depicts the experimental set-up. The inox tube positioned above the laser prevented air turbulence caused by the cooling system perturbing the photo-writing process. The UV beam emitted by the laser was reflected by four mirrors (even number of reflections to preserve the output state of polarization) towards the POF, which was held in a V-groove plate. A uniform phase mask (Coherent) with a period of 1044 nm was placed above the fiber as closely as possible. A cylindrical lens with 10 cm focal length was used upstream of the phase mask to focus the UV beam on the fiber core. The movement of the third mirror was controlled by a motor-driven translation stage, which was used to scan the laser along the fiber over a maximum length of 20 mm. Amplitude reflected spectrum measurements were obtained with an FBG interrogator (FS2200SA from FiberSensing), which presents a wavelength resolution of 1 pm and a scanning rate of 1 Hz. MPOFBGs were fabricated at Aston University using a He-Cd laser (Kimmon IK3301R-G) and the experimental set-up is similar to the one described above.

3. PDL AND DGD MEASUREMENTS FOR UV-INDUCED FBGS

3.1 PDL and DGD measurements for step-index POFBGs

The reflective FBGs in POF were measured in transmission with polarized light. We have used an optical vector analyzer (OVA CTe from Luna Technologies) that was chosen for both its high wavelength resolution (1.25 pm) and its fast scanning rate (less than 1 s to analyze a range of a few tens of nm). Figure 2 depicts the spectra of transmission, PDL and DGD measured by the OVA. By measuring the transmitted amplitude spectrum, the maximum reflectivity has been
computed equal to 97%. The maximum value of PDL is equal to 0.9 dB above noise level. The latter is close to 1 dB and is essentially due to the splices. The photo-induced birefringence value is estimated through a numerical fit of the experimental data, using an in-house developed inverse scattering program based on the Nelder-Mead simplex algorithm \(^2^7\). The birefringence has been estimated to \(7 \times 10^{-6}\). The maximum value of DGD is 3.3 ps above noise level. Thus, this measurement confirms that the side inscription process induces non-negligible photo-induced birefringence in step-index POFBGs, as in the case of silica fibers \(^2^5,^2^6\).

3.2 PDL and DGD measurements for mPOFBGs

Similar measurements were conducted for mPOFBGs. Figure 3 depicts the transmitted spectrum, PDL and DGD curves of a grating with a reflectivity of 86%. Here, the maximum values of PDL and DGD are 4.8 dB and 9 ps above noise level, respectively, confirming that photo-induced birefringence is also present for this mPOF. The irregular evolution at the left side of the rejection band is attributed to the fibre being few-moded in this wavelength range.

![Figure 2. Transmitted spectrum (a), polarization dependent loss (b) and differential group delay (c) for a 6 mm long step-index POFBG.](image-url)

![Figure 3. Transmitted spectrum (a), polarization dependent loss (b) and differential group delay (c) for a 5 mm long mPOFBG.](image-url)
4. TRANSVERSE FORCE MEASUREMENT

In this section, we make use of the PDL values for transverse force sensing purposes. In our set-up, two 20 mm long POFs with and without grating, respectively, were placed parallel and pressed between two metal plates, which avoided the tilt of the loading area. The loads were applied and varied on the top of the plate in the range (0 - 0.75 N) for each fiber. Figure 4 depicts the evolution of the PDL maximum value as a function of the transverse force. It can be seen that the evolution is linear in that range. A linear regression of the raw data yields a maximum PDL value sensitivity equal to 1.7 dB/N ± 0.2 dB/N.

![Figure 4. PDL evolution as a function of transverse force for a 6 mm long step-index POFBG.](image)

5. CONCLUSION

(M)POFBGs were photo-written by UV laser at the wavelength of 325nm. Then the transmitted amplitude spectra, PDL and DGD curves were measured by an optical vector analyzer. For step-index POFBGs, the reflectivity is 97 % and the maximum values of PDL and DGD are equal to 0.9 dB and 3.3 ps, respectively. By transverse force measurement, the PDL sensitivity is calculated to be 1.7 dB/N. As for mPOFBGs, the reflectivity is 86 % and the maximum values of PDL and DGD are equal to 4.8 dB and 9 ps, respectively. This preliminary study about birefringence effects in POFBGs confirms the great potential that such measurements can have for transverse strain sensing.

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